

Innovative calibration procedure of numerical models for FOWTs: an experimental validation

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1 Introduction

Numerical modeling of the floating offshore wind turbine (FOWT) dynamics plays a critical role at the design stage of a floating wind project. The relevance of these models depends on how they correspond to the **real-life situation**; specifically, prediction of the **platform motions** in the **wave** and **resonance** frequency bands is challenging.

2 Numerical modeling of the FOWT

Equation of motion: Cummins' equation

$$(M + A_\infty) \cdot \ddot{x}(t) + \int_0^\infty B_r(\tau) \cdot \dot{x}(t - \tau) \cdot d\tau + C \cdot x(t) = F_{ext} \quad (1)$$

M Mass matrix

A_∞ Added mass matrix at ∞ frequency

B_r Retardation function

C Restoring (hydrostatic) matrix

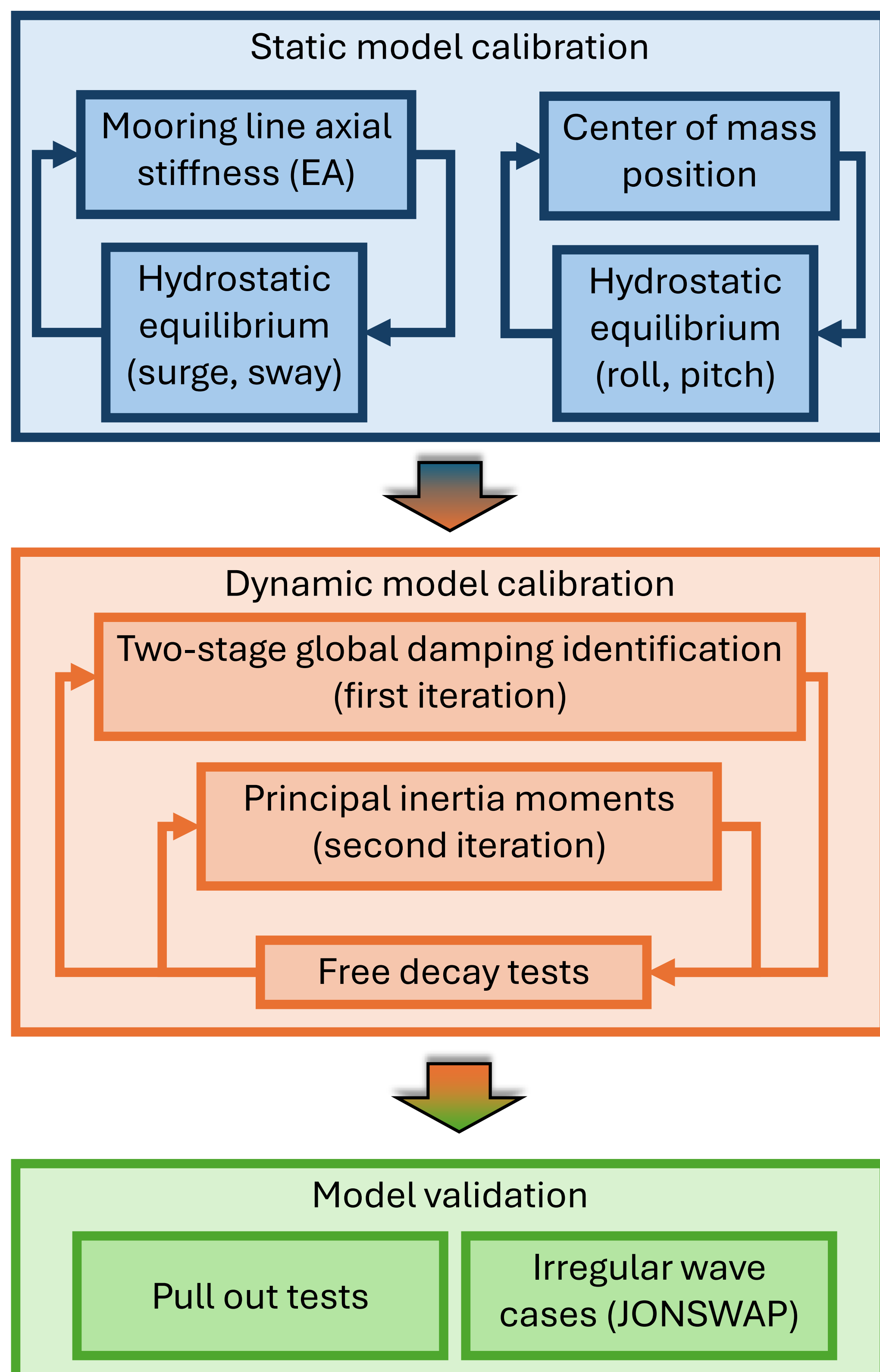
x Platform motions vector

F_{ext} External loads vector: wave excitation and mooring loads

Hydrodynamic and mooring loads

- Second order potential flow theory
- Full mean and low-frequency wave drift loads
- Global linear and quadratic viscous damping matrices
- Lumped mass model with linear stiffness

3 Model calibration

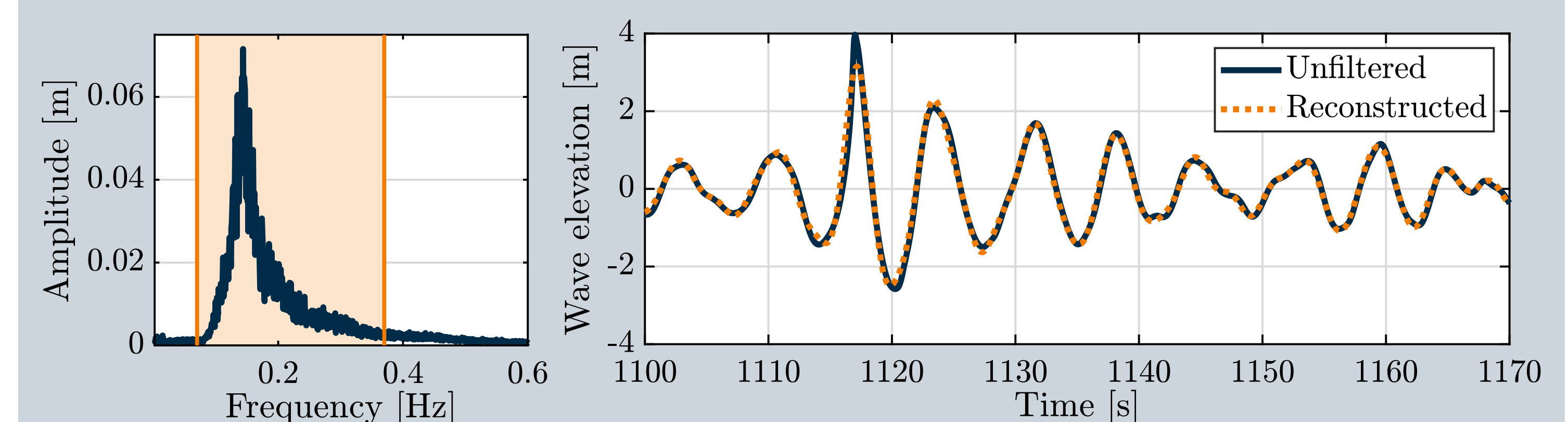


4 Model validation

Pre-processing of wave input

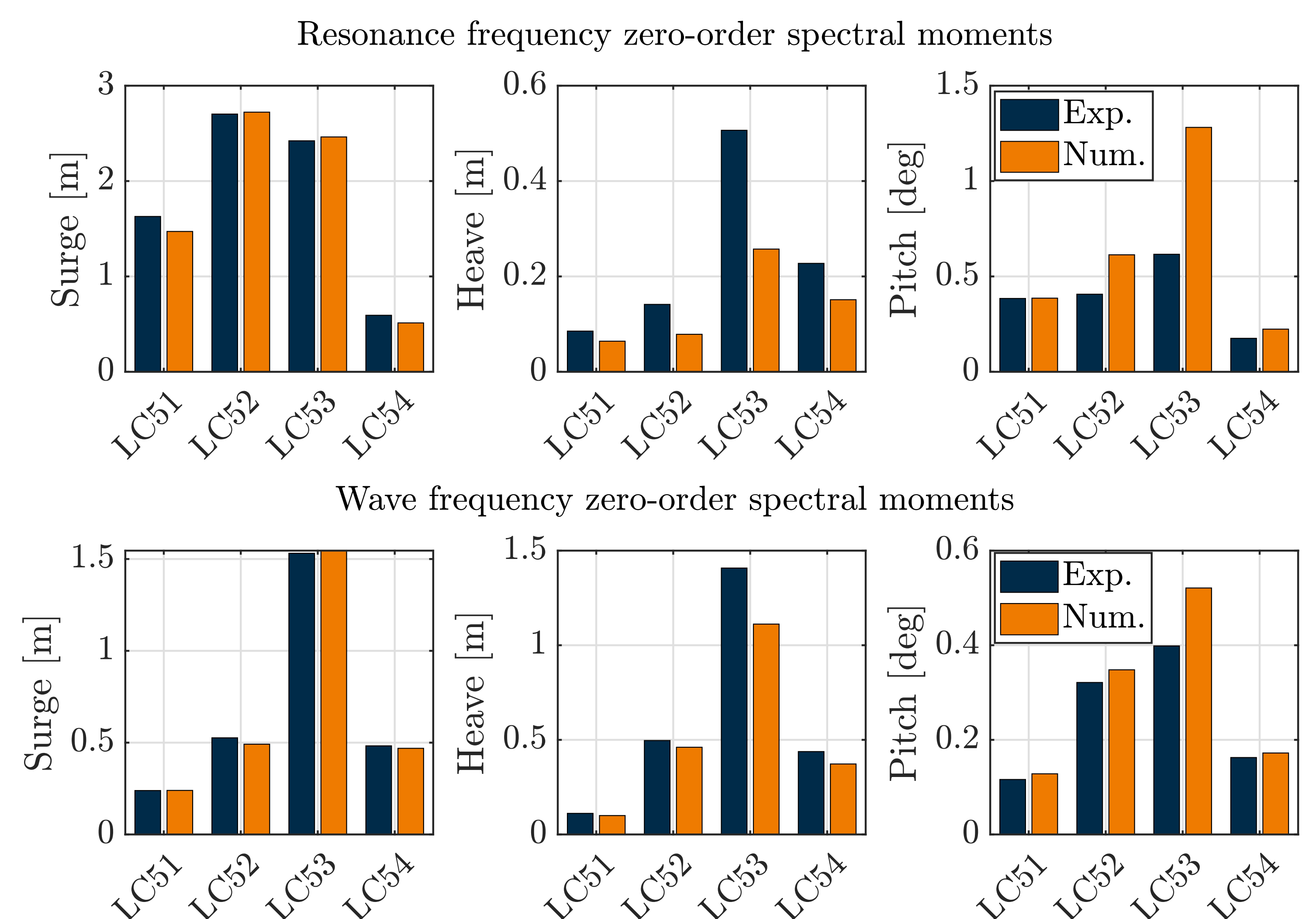
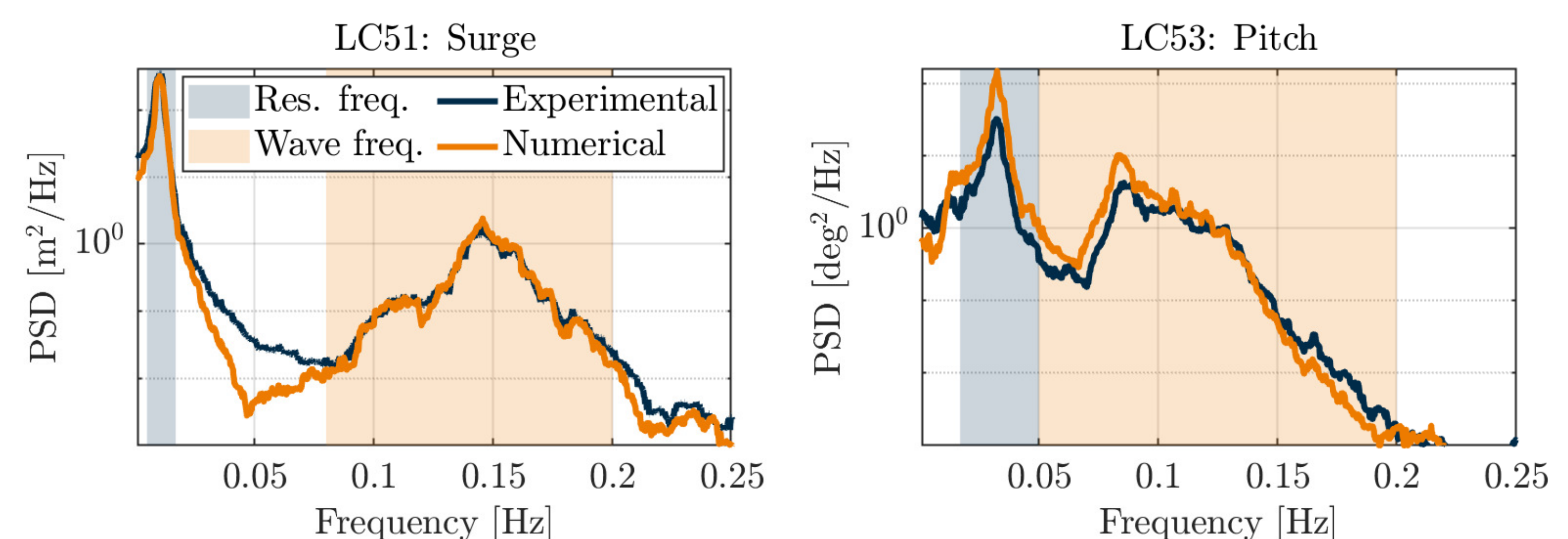
Pass-band filtering of the wave spectrum:

- Reduction of the **number of components**
- **Speeding-up** of the simulations



Model validation under four different irregular waves by comparing:

- Power spectral densities (PSDs)
- Zero-order spectral moments over **resonance** frequency band
- Zero-order spectral moments over **wave** frequency band



5 Conclusion

Systematic tuning of the numerical model of the semi-submersible yields **better prediction** of the platform's motions. The relatively computationally inexpensive proposed calibration procedure shows some limitations in the prediction of the **low-frequency motions**. Therefore, it is suggested to always include and calibrate **Morison drag coefficients** for the slender elements of semi-submersible structures for FOWTs.