

Blade Surface Pressure Measurements in the Field

and their usage for aerodynamic model validation

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Importance of aerodynamic field measurements

Background and motivation

- Since 80s there have been joint efforts to validate and improve rotor aerodynamic models (IEA TCP Wind)
- With the advent of larger rotors, the topic of efficient but accurate models remains work in progress
- It is acknowledged that detailed sectional aerodynamic measurements (such as blade surface pressures) are needed to advance, a.o. to prevent compensating errors from integral measurements
- The wind energy community lacks publications featuring field databases of representative scale and measurement duration for this purpose
- Can we tackle this shortcoming??



Outline

Overview

- Background and motivation
- Methodology
 - Test set-up
 - Simulations
- Results
 - Pressure measurements
 - Comparison to simulations
- Conclusions and recommendations



Project overview

TIADE (Turbine Improvements for Additional Energy)

2020 - 2024



Scope of TIADE project:

- Blade improvement (innovative tip shapes, VGs, turbulator tips)
- Validation (erosion, yawed inflow, stall and/or vortex induced vibrations)
- Measurement innovations (aerodynamic pressure, torsion deformation, fibre optics)

K. Boorsma et al, *TIADE final report*, TNO-2024-R12112, December 2024,
<https://publications.tno.nl/publication/34643564/vPzmF6yO/TNO-2024-R12112.pdf>

TIADE has partly been financed with Topsector Energiesubsidie from the Dutch Ministry of Economic Affairs under grant no. TEHE119018

Test set-up

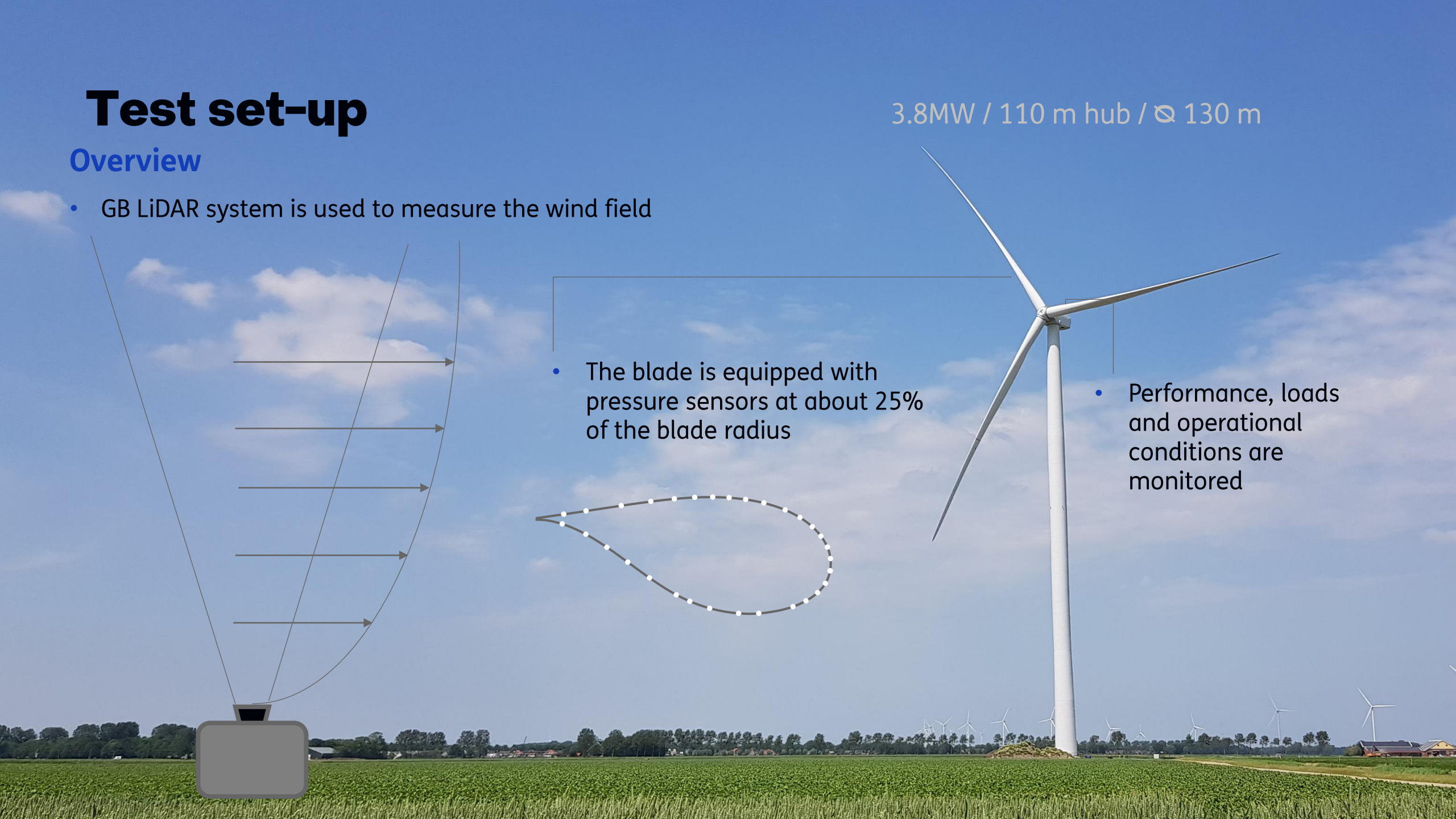
Overview

- GB LiDAR system is used to measure the wind field

3.8MW / 110 m hub / \varnothing 130 m

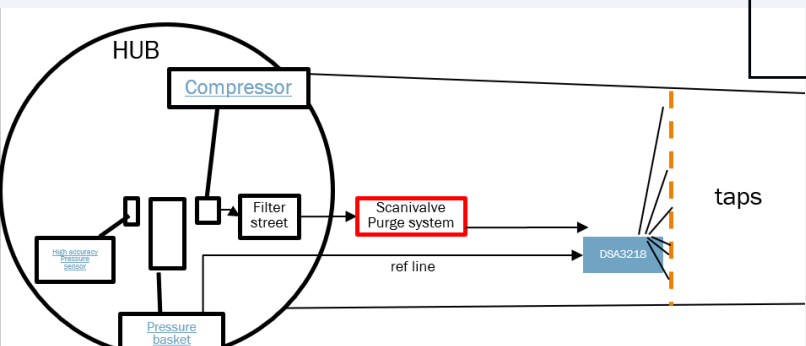
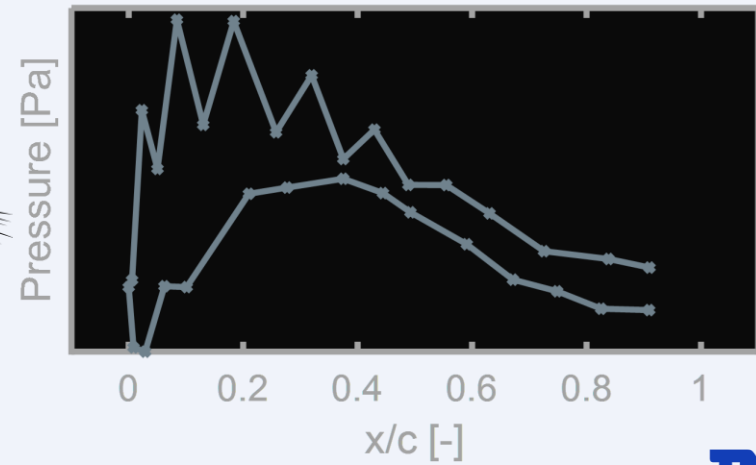
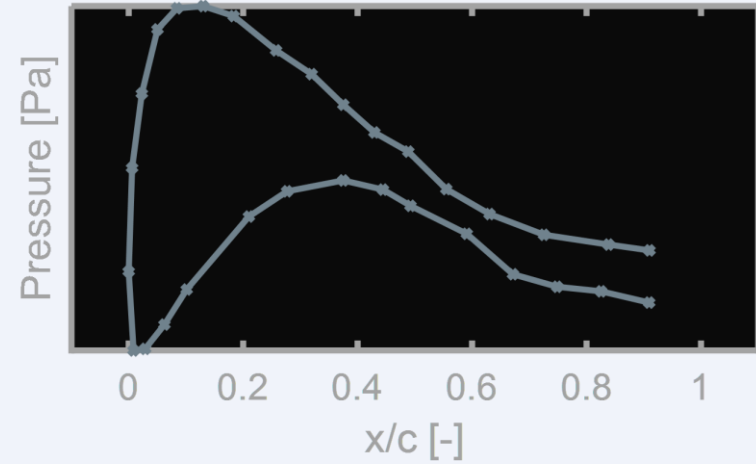
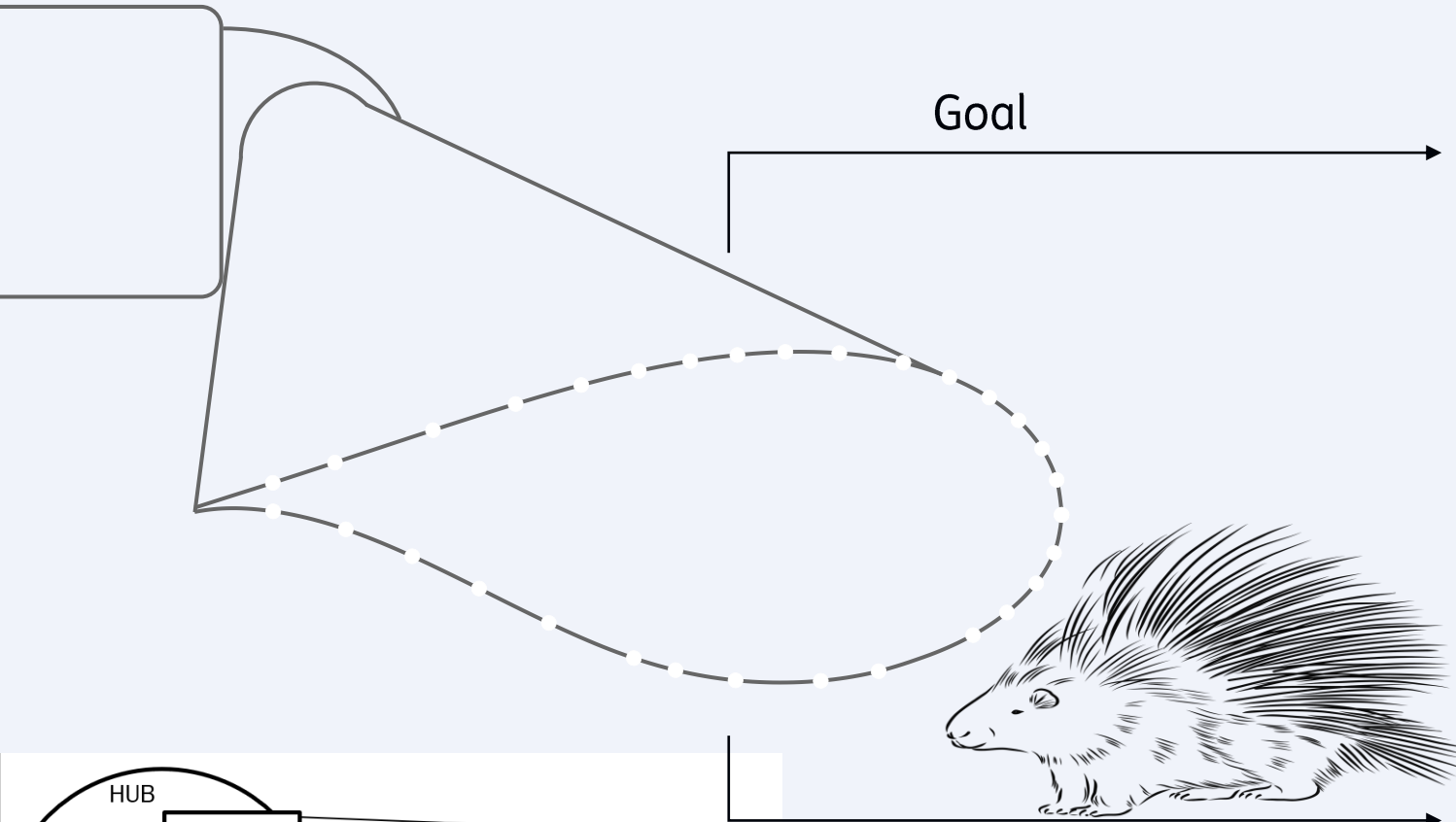
- The blade is equipped with pressure sensors at about 25% of the blade radius

- Performance, loads and operational conditions are monitored



Test set-up

Challenges



Numerical simulations

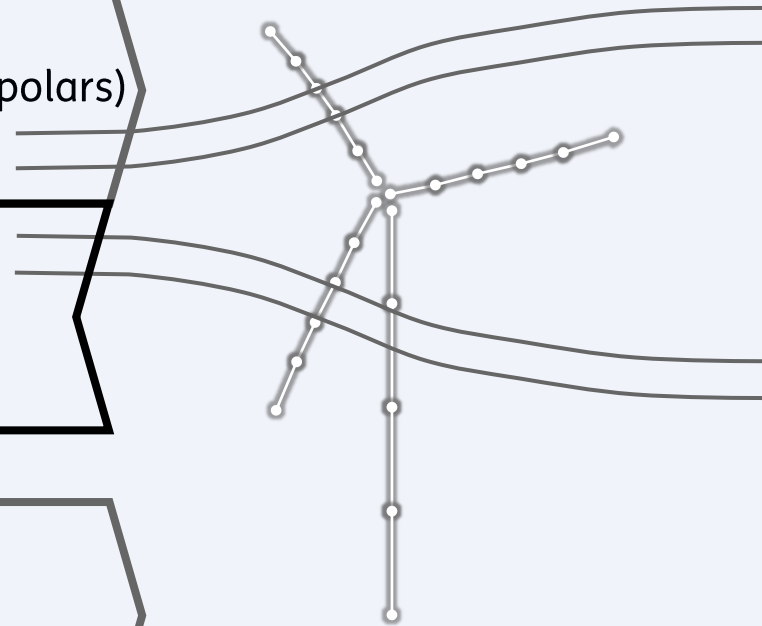
Simulation tools

Input:

- Aerodynamic and structural turbine model (wind tunnel polars)
- Operating conditions

Output:

- Power, thrust
- Blade aerodynamics, moments and deformations



Phatas

- BEM
- Structural solver

Input:

- Airfoil geometry
- Reynolds number, Angle of attack, c/r value

Output:

- Airfoil polars: c_l , c_d , c_m
- Pressure coefficient distribution

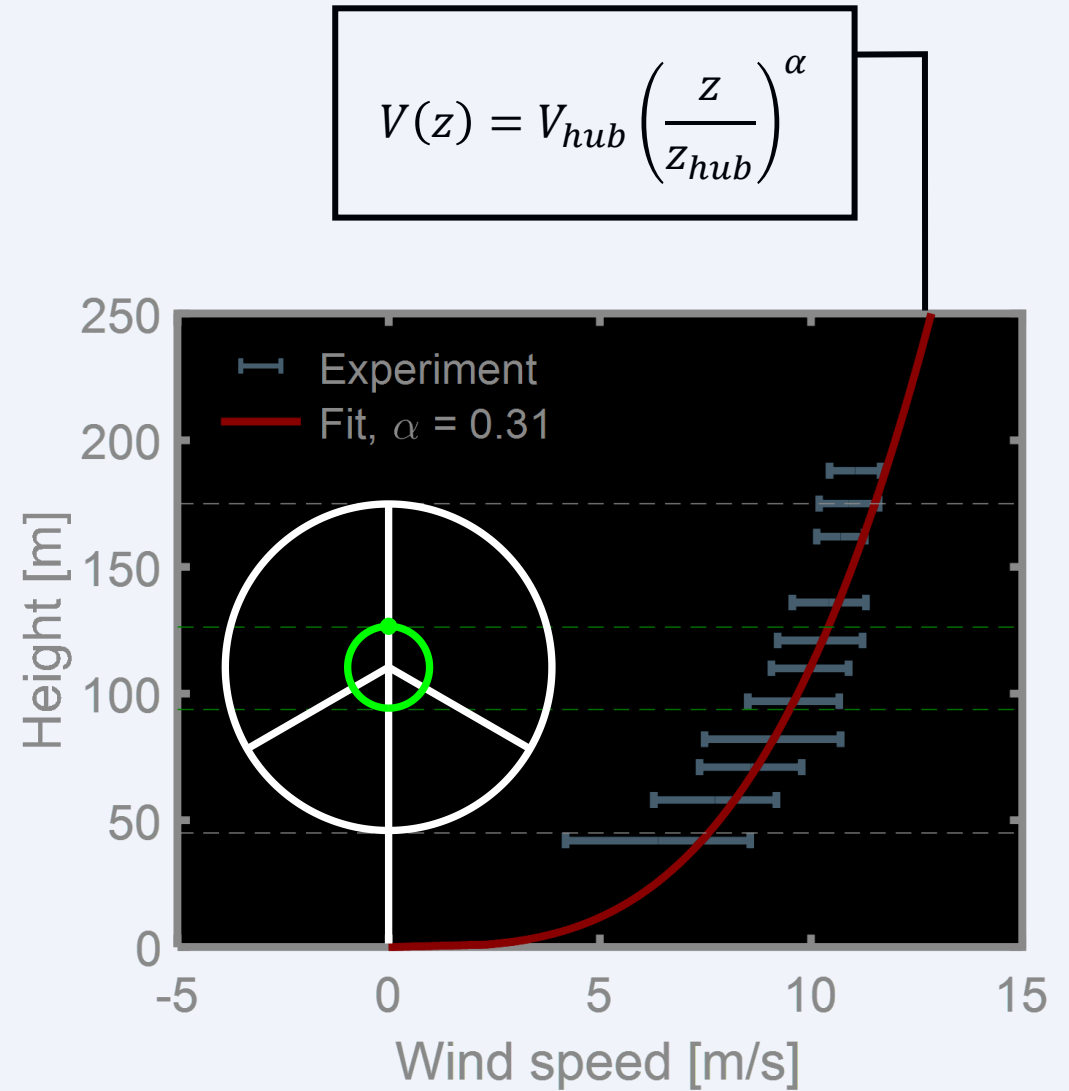
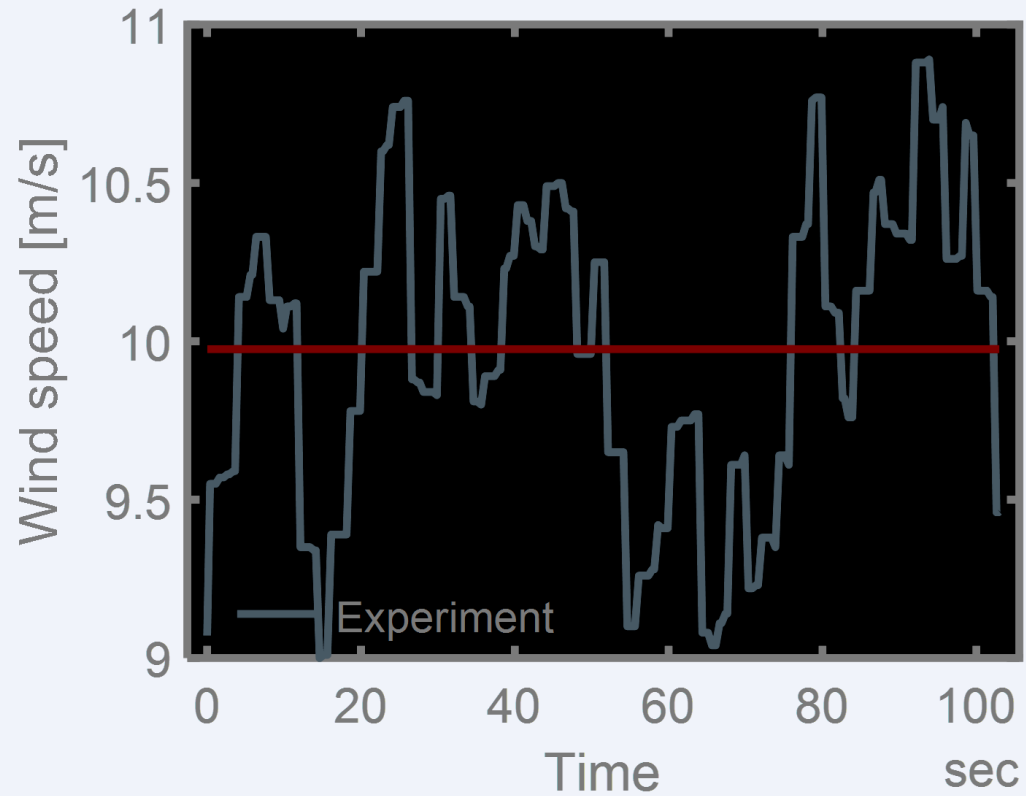


RFOIL

- 2D panel method
- Based on XFOIL
- Modified for rotating airfoils

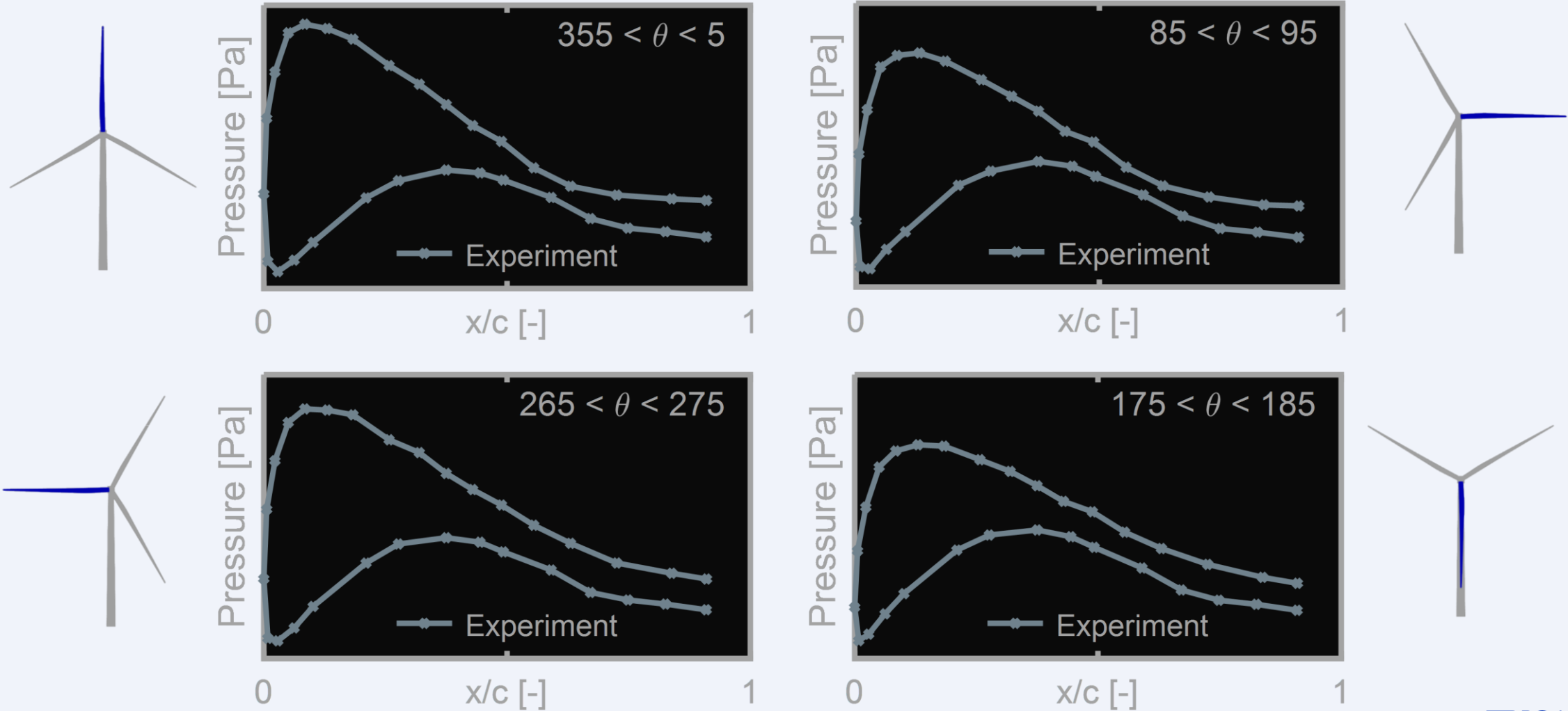
Results

Operational conditions



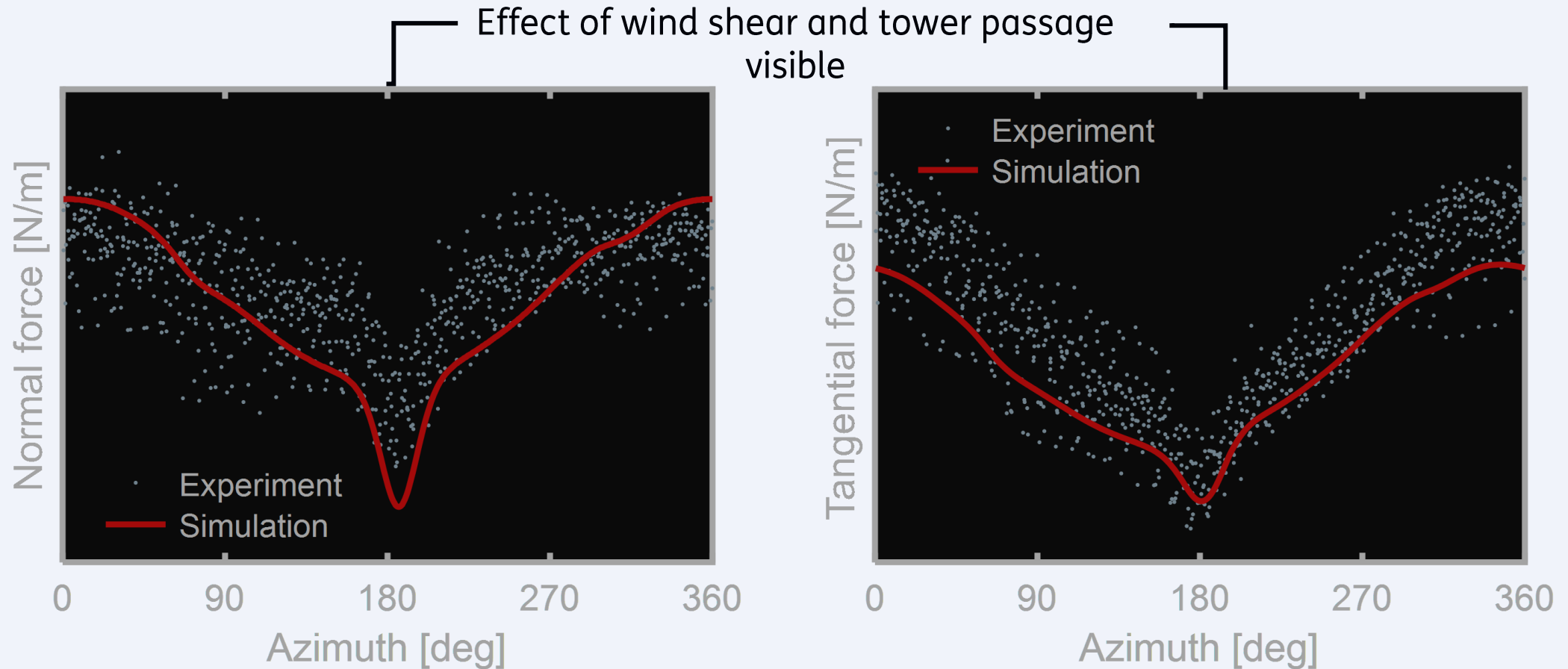
Results

Pressure distribution variation over a rotation



Results

Sectional forces



Results

Obtaining trends

Filter samples of 10-minute statistics for

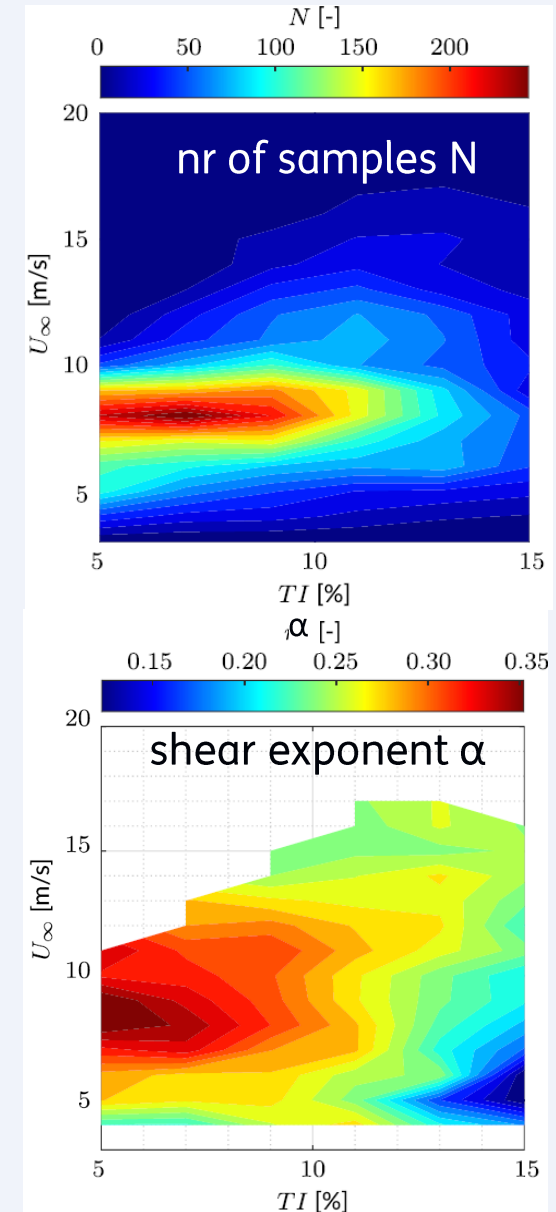
- Normal operating conditions (no standstill)
- Undisturbed wind sector (no waked inflow)
- No extreme events (exclude large yaw misalignment, TI and shear)
- Malfunctioning sensors

~10% of data remains

Bin average the resulting samples

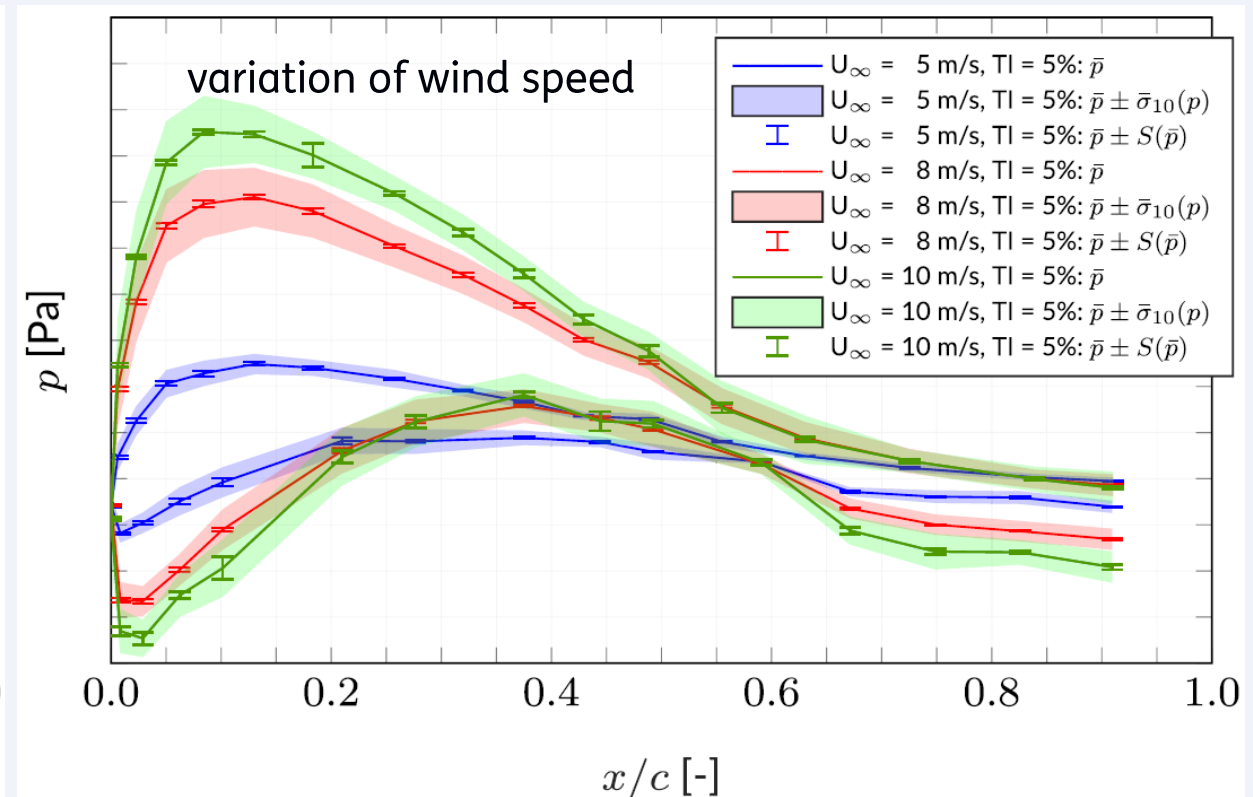
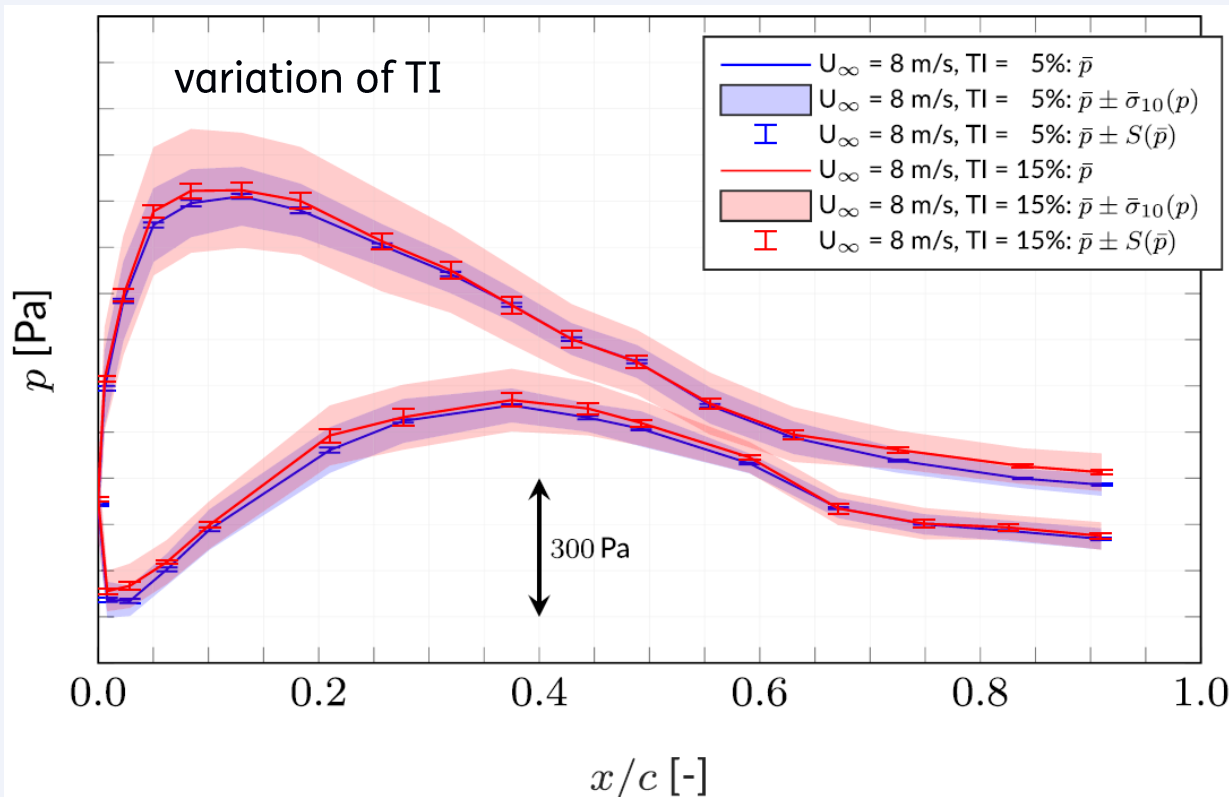
- Wind speed 3 to 20 m/s in steps of 1 m/s
- TI between 5% to 15% in steps of 2%
- Exclude bins < 6 samples
- Standard error to observe repeatability

$$S(\bar{\xi}) = \frac{\sigma_{bin}(\bar{\xi})}{\sqrt{N}}$$



Results

Trends: Variation with wind speed and TI



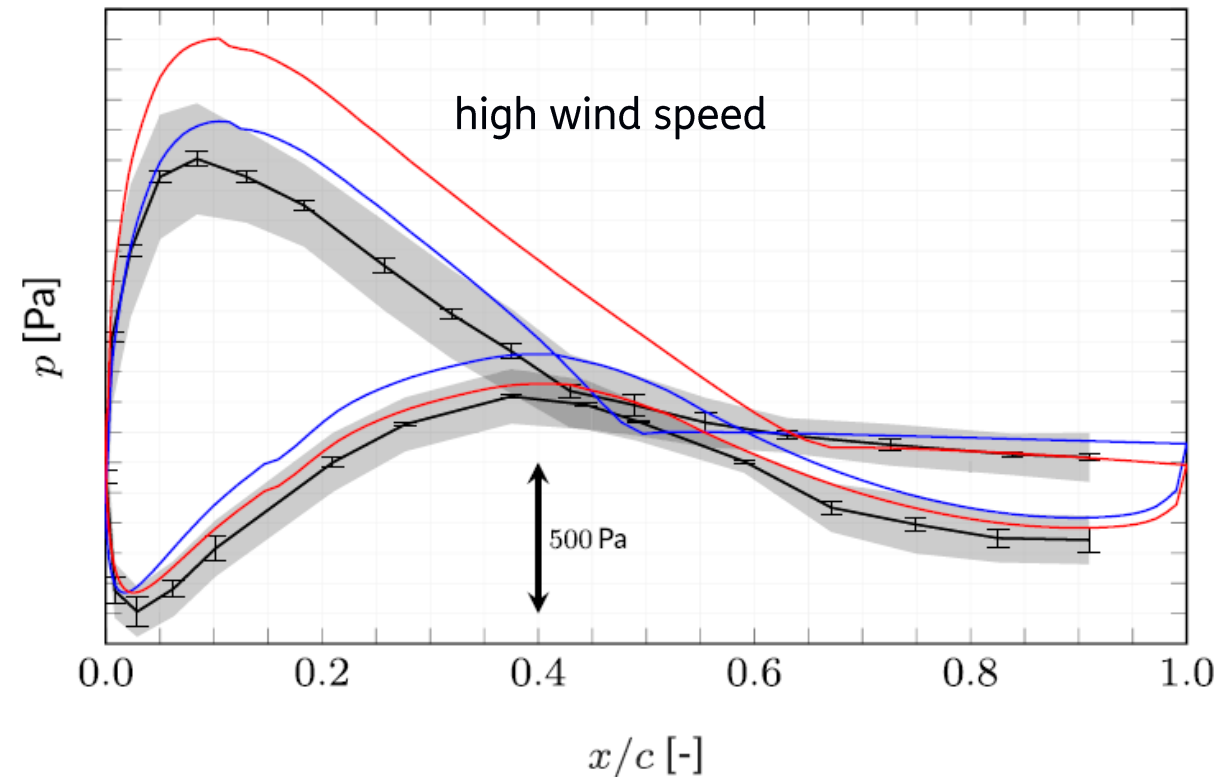
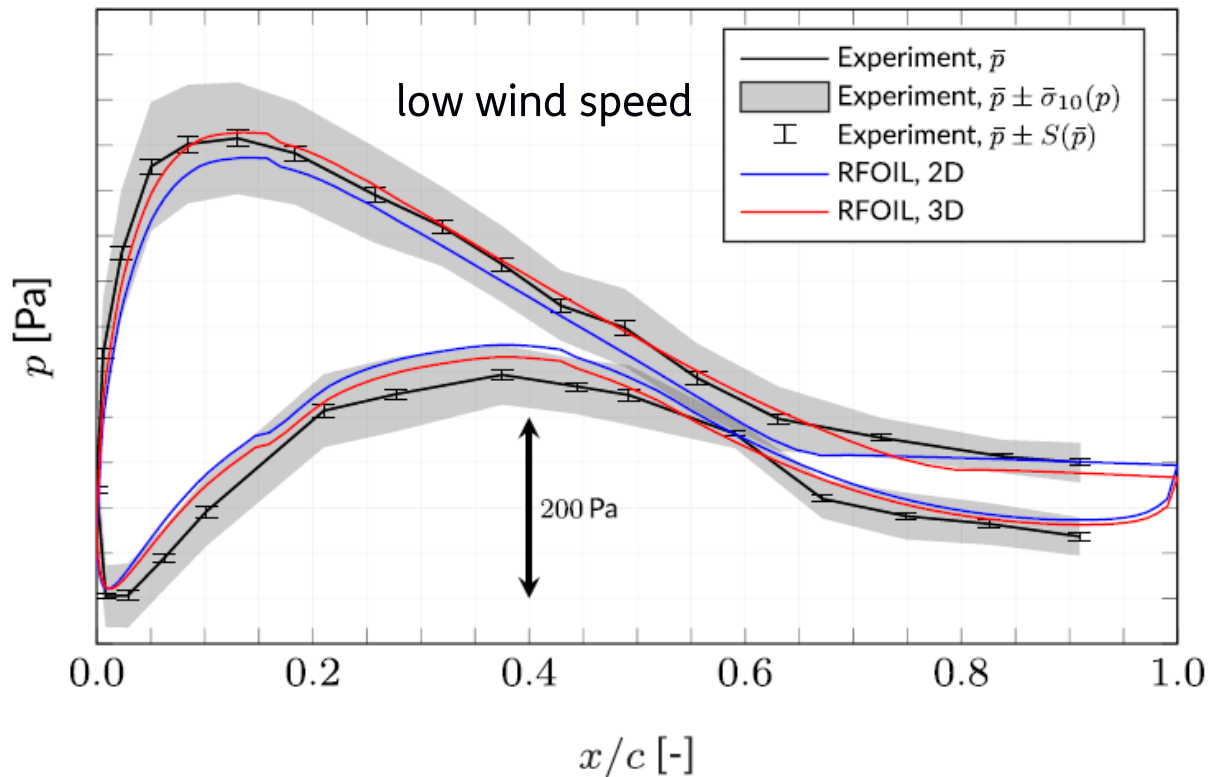
Results

Comparison to RFOIL – pressure distribution

- Input bin avg operational conditions to Phatas to obtain sectional conditions
- Input AOA and Re to RFOIL

$U_\infty = 6 \text{ m/s}$, $\alpha = 7.52^\circ$, $Re = 4.13E6$, $N_{crit} = 0.69$

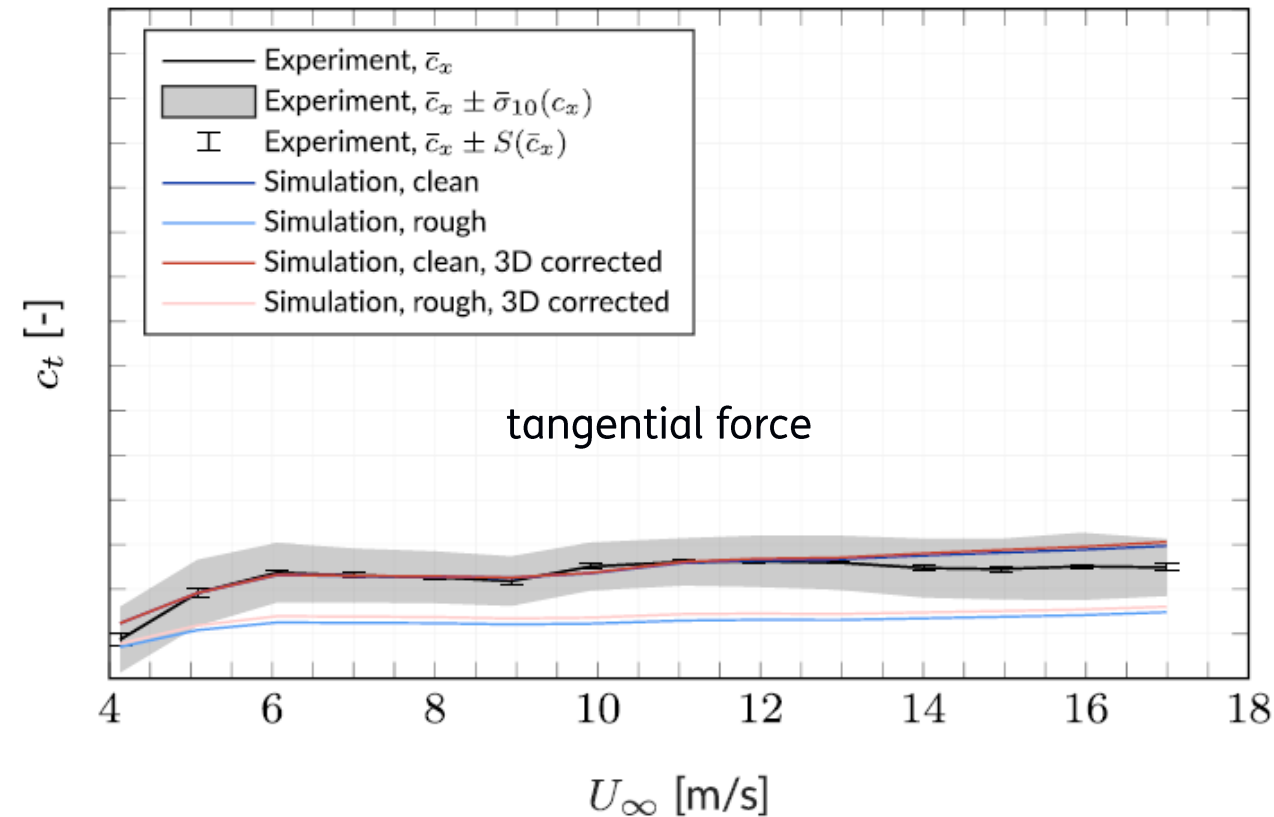
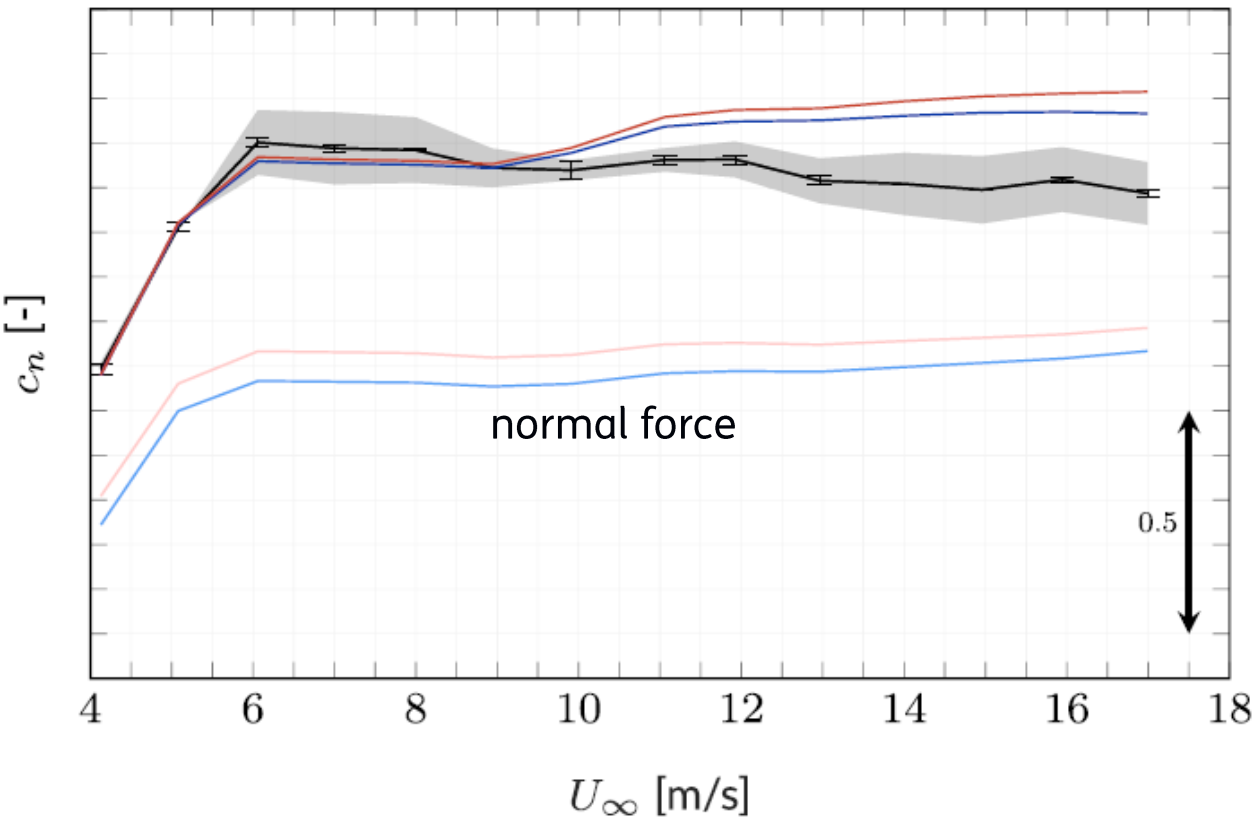
$U_\infty = 17 \text{ m/s}$, $\alpha = 11.24^\circ$, $Re = 7.26E6$, $N_{crit} = 0.47$



Results

Comparison to Phatas – normal and tangential force (steady)

- Measured and simulated coefficients non-dimensionalized without induced velocities





Conclusions and recommendations

- Blade surface pressures were successfully measured on a state of the art R&D 3.8 MW wind turbine over a 2 year period, providing invaluable means for validating design tools
- The resulting measurement database gives a good insight in the aerodynamic performance at the measured section
- Overall a reasonable agreement has been obtained between numerical simulations and field experiments
 - Numerical tools based on blade element momentum theory and panel methods with viscous-inviscid interaction remain relevant for simulating modern multi-megawatt wind turbines
 - Larger discrepancies can be observed for higher wind speeds, when stalled flow occurs
- More details and results, e.g. about correlation with unsteady simulations, in the dedicated publication: E. Fritz et al, *Blade Surface Pressure Measurements in the Field and Their Usage for Aerodynamic Model Validation*. Wind Energy 27(12), December 2024, <https://doi.org/10.1002/we.2952>

A nighttime photograph of a city street. In the foreground, a modern, curved pedestrian bridge with a glass railing and a perforated metal mesh base spans across the street. The bridge is illuminated from below, creating a warm glow. In the background, several multi-story buildings are visible, with many windows lit up. A prominent feature is a long, horizontal light trail in a vibrant green color, which appears to be a light rail or tram moving across the frame. The overall scene is a blend of urban architecture and modern transportation technology.

› **Thank you for your attention**

Take a look:

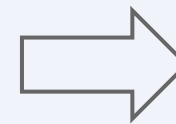
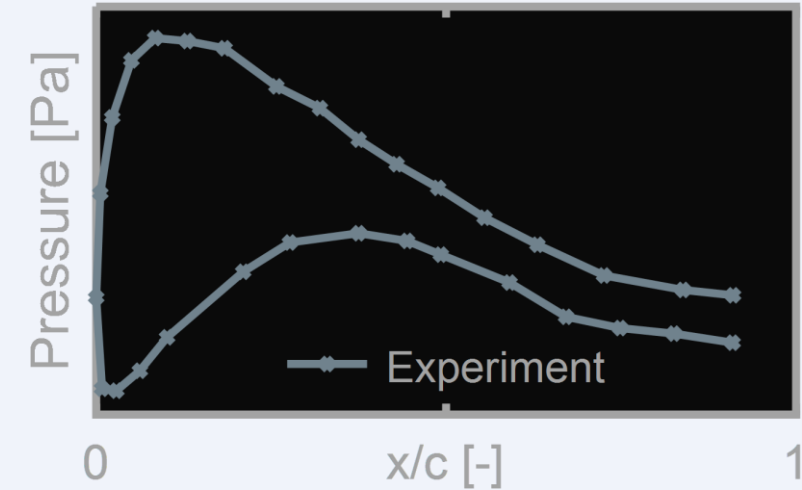
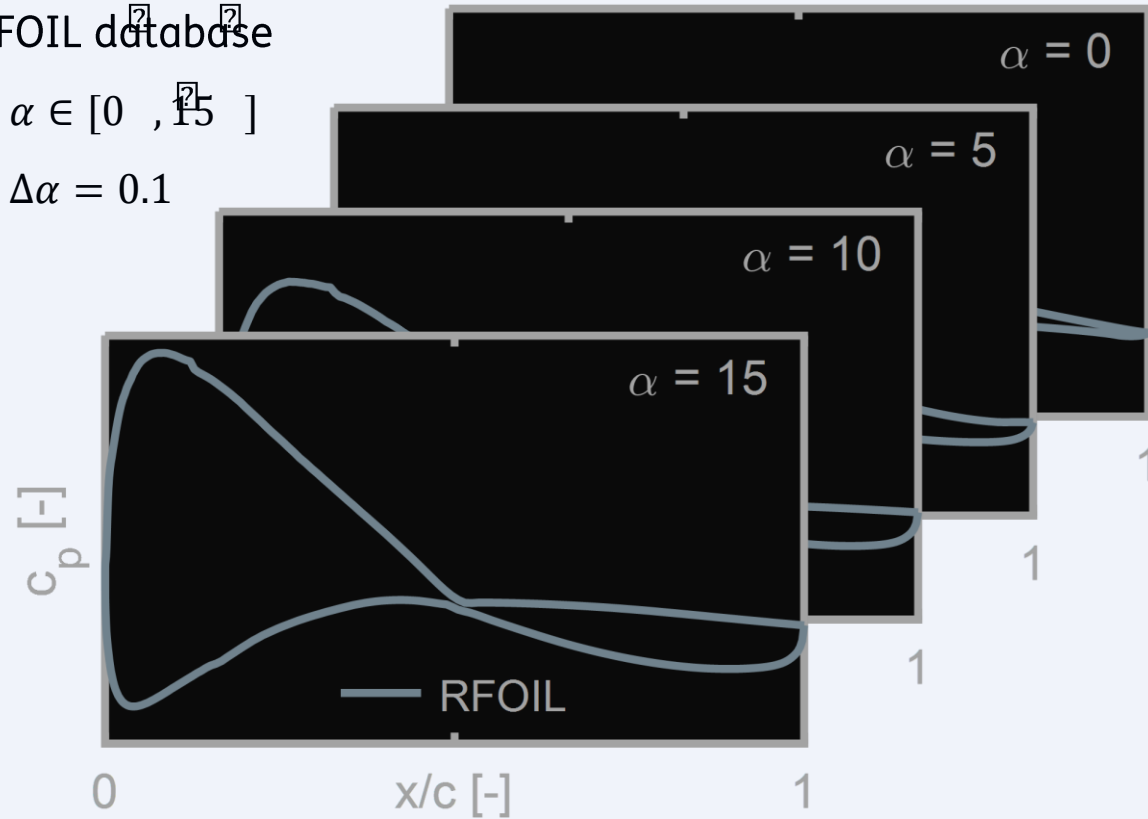
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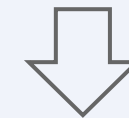
Results

Angle of attack estimation

- RFOIL database
- $\alpha \in [0, 15]$
- $\Delta\alpha = 0.1$



Pattern matching

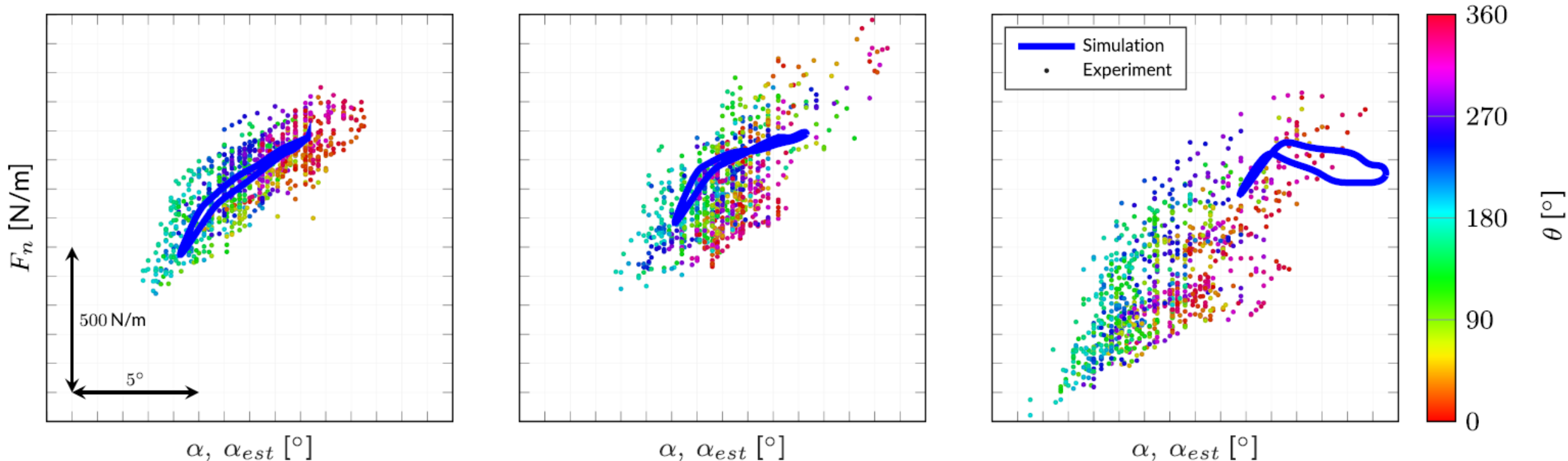


Angle of attack estimation

Results

Comparison to Phatas – normal force (unsteady loops)

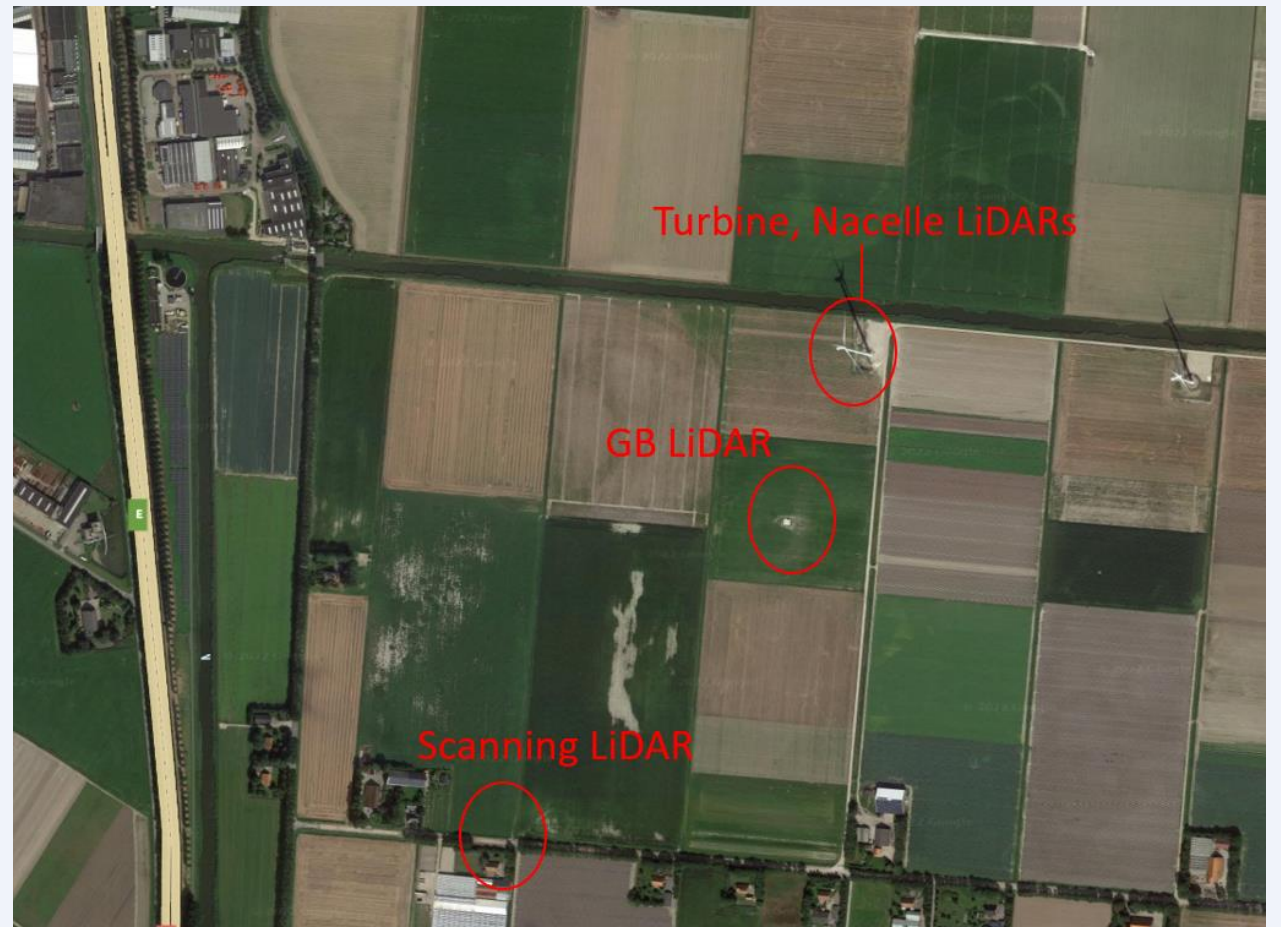
- Measurements: Estimated angle of attack α_{est} using pattern matching
- Simulations: Snel 1st order dynamic stall
- Agreement between measurements and simulation varies between samples



Test set-up

Test site overview

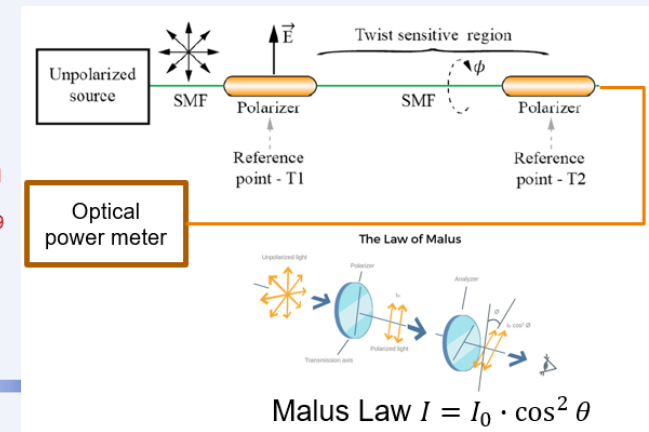
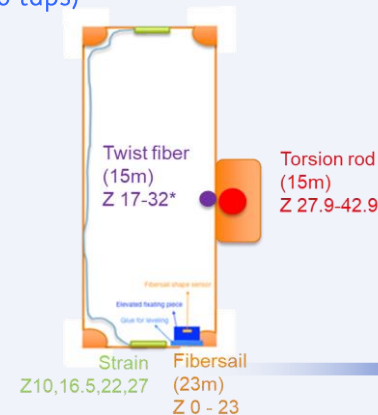
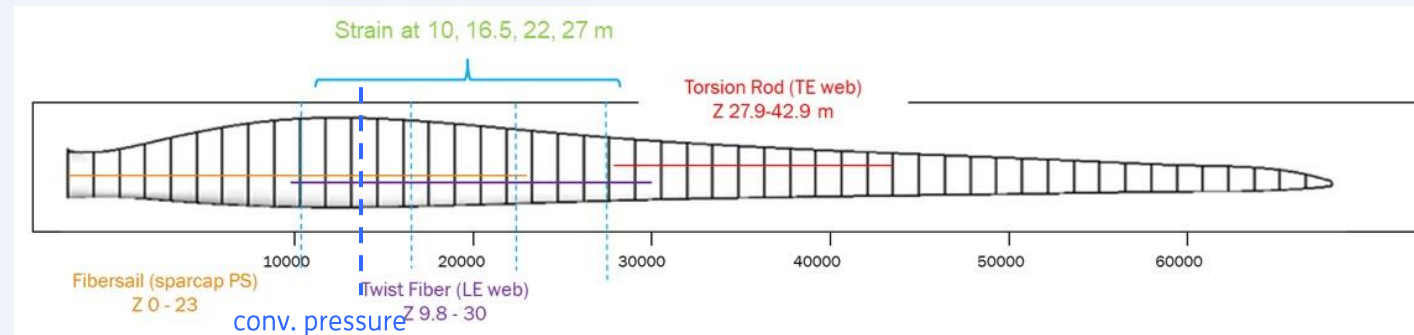
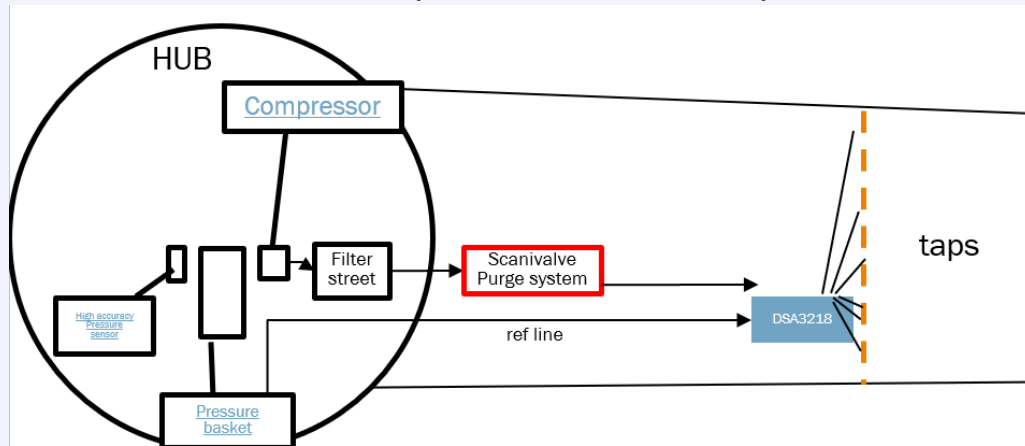
- Turbine type: 3.8MW, 110 m hub height, 130 m rotor diameter
- Ground based Windcube LiDAR @ 11 heights (42 - 188 m)
- 2 Nacelle based fwd looking LiDARs (~0.25D - 5D)
- Meteo mast at 2 km from turbine (wind, press, temp, disdro)
- Scanning LiDAR to measure wake at hub height (1D - 5D)



Test set-up

Turbine instrumentation

- IEC compliant power performance and loads (tower/shaft/blade)
- SCADA and tower top acceleration/inclination
- Deformation (torsion / flap / edge) and tufts @ blade roots
- Conventional pressure (+ fibre optic trial) @ 25% r/R (~2 years!)

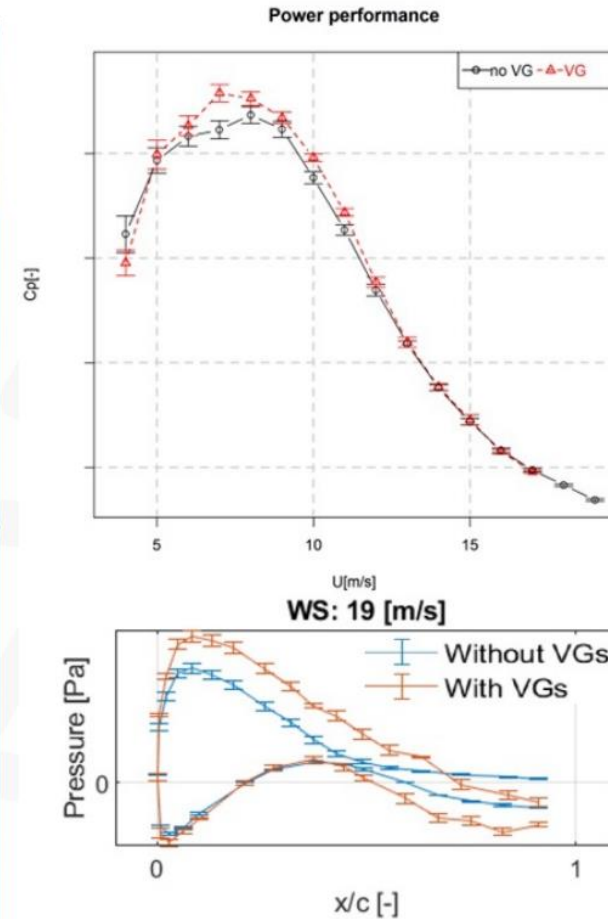


Effect of Vortex Generators

Vortex generators



(a) Installation of VGs using rope access



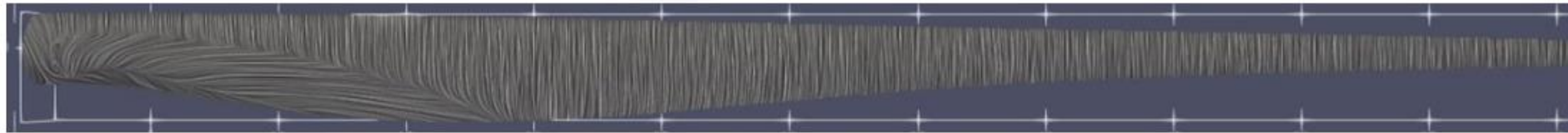
(b) Measured power coefficients (above) and pressure distributions (below) with and without VGs [19]

[18] K. Vimalakanthan. *Vortex generator layout design for TIADE blade section at 15m blade span*. Tech. rep. TNO 2024 R12151. TNO, 2024.

[19] G. Vanino. *Vortex Generators applied to large-scale Wind Turbines*. Tech. rep. TNO 2023 M12095. TNO, 2023.

Validation of models

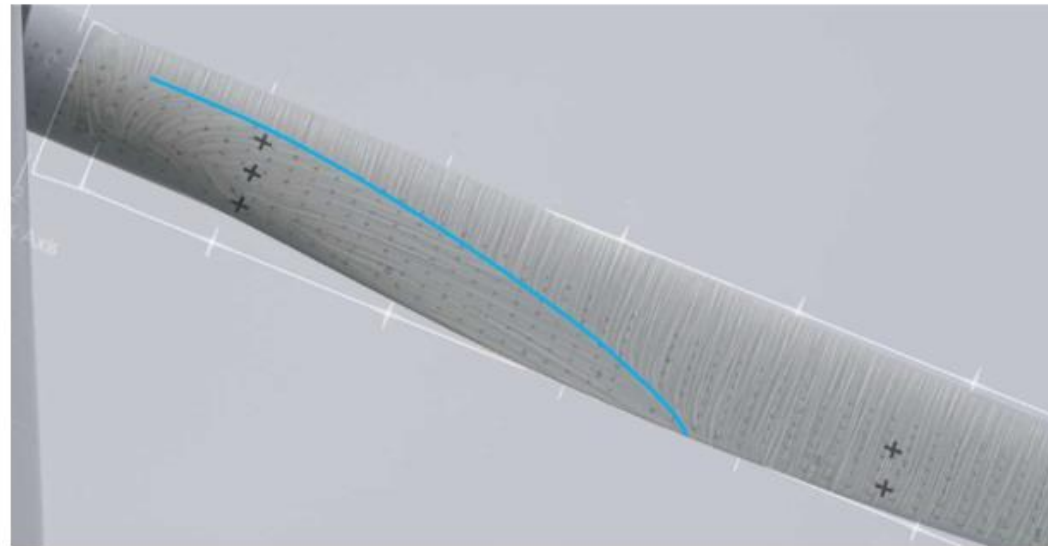
Tuft measurements



(a) Simulated streamlines from CFD



(b) Tuft visualization with separation line in blue



(c) Overlay of tuft and CFD results

Figure 3.11: Comparison between measured and predicted streamlines using tufts visualization and CFD simulations at 8 m/s [13]

[13] M. Caboni et al. *3D RANS-based CFD simulations on the LM637P blade*. Tech. rep. TNO 2024 M11257. TNO, Nov. 2024.